



# Very Large Wind Farm Design Improvement Using Multi-Fidelity Modelling Approaches

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An extended theoretical model, which is based on a generalised two-scale coupled momentum conservation argument, is proposed to estimate aerodynamic effects of support structures on the performance of ideal very large wind farms. The model suggests that the parameter  $(A_s/A) \cdot C_D^*$ , which represents an effective support-structure drag, plays an important role in the design and optimisation of very large wind farms. To validate this extended model, Detached-Eddy-Simulations (original version with Spalart-Allmaras model) of a periodic staggered array of actuator discs with and without support structures are conducted.

Based on original model (Nishino 2016)

$$\langle \tau_w \rangle S + T + D = \frac{\Delta p}{\Delta p_0} \tau_{w0} S$$

$$T = \frac{1}{2} \rho U_F^2 A \cdot C_T^*$$

$$D = \frac{1}{2} \rho U_F^2 A_s \cdot C_D^*$$

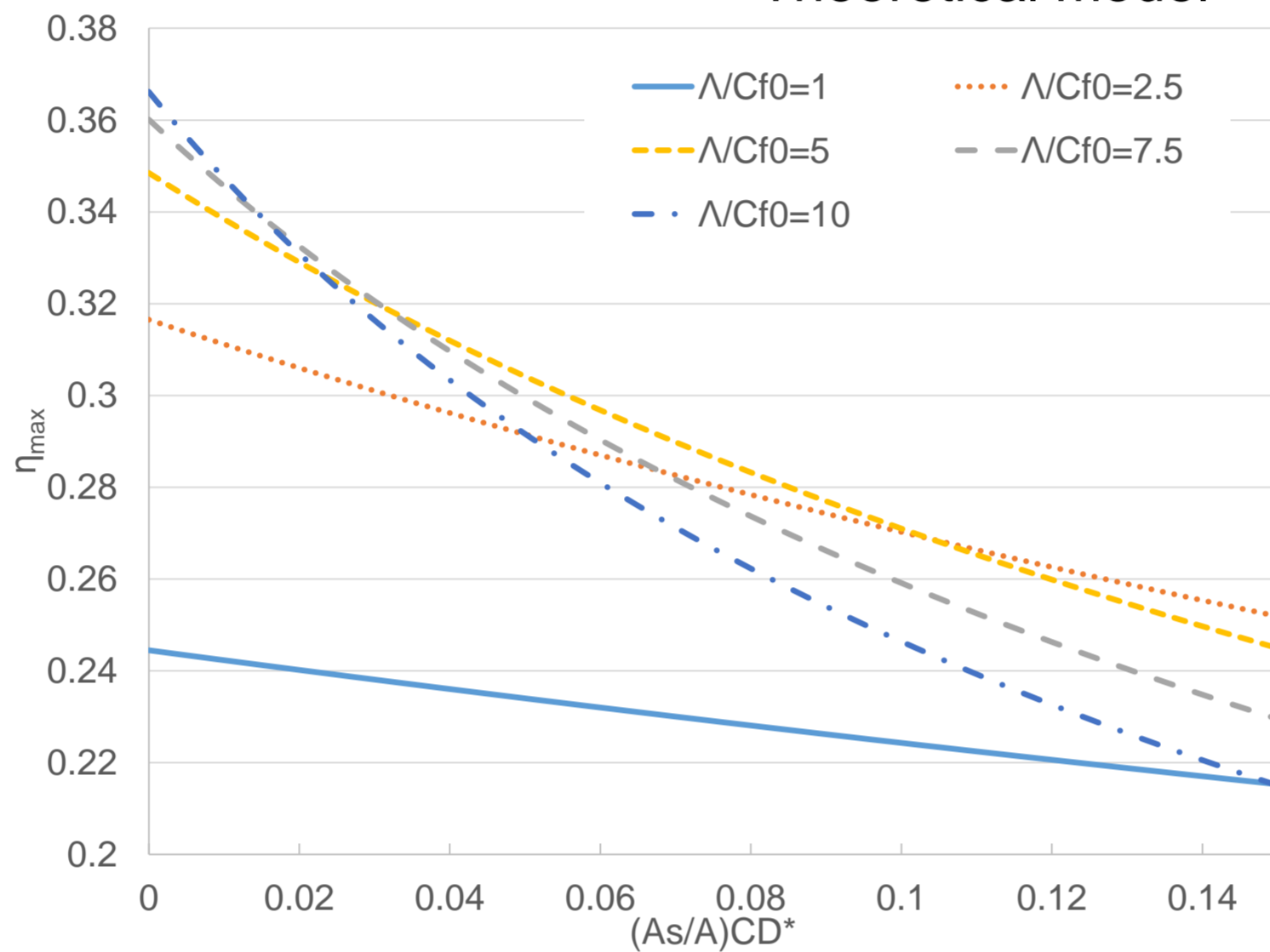
Generalised two-scale coupled momentum equation

$$\frac{\Lambda}{C_{f0}} \cdot \beta^2 \cdot \left( 4\alpha(1-\alpha) + \frac{A_s}{A} C_D^* \right) - 1 + \beta^\gamma = \zeta(1-\beta)$$

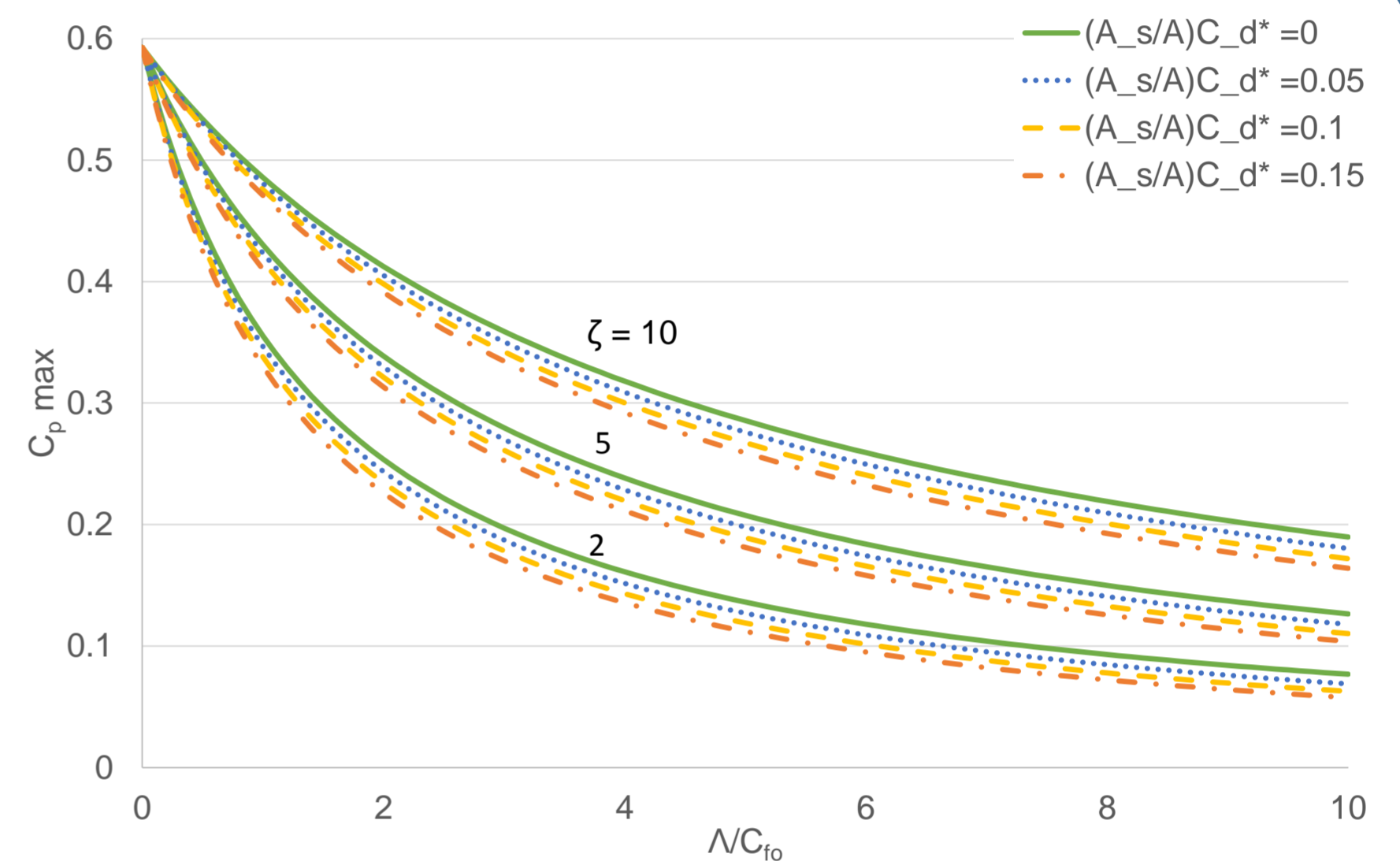
Normalised power density

$$\eta = \frac{\text{Power}}{\tau_{w0} U_{F0} S} = \frac{\frac{1}{2} \rho U_{F0}^3 A C_P}{\tau_{w0} U_{F0} S} = \Lambda \cdot \frac{1}{C_{f0}} \cdot C_P = \Lambda \cdot \frac{1}{C_{f0}} \cdot 4\alpha^2(1-\alpha)\beta^3$$

Theoretical model

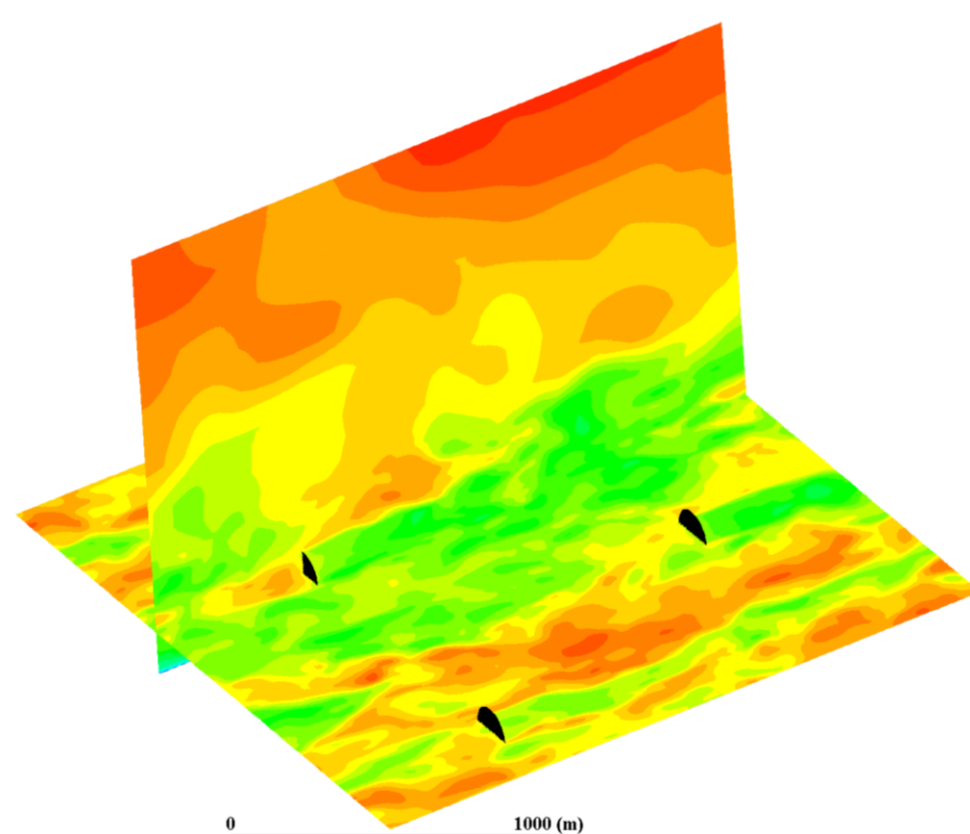
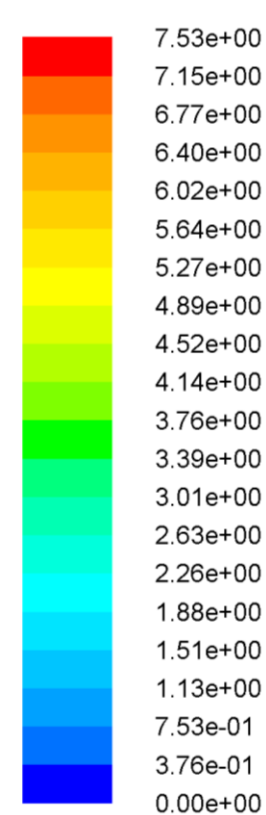


The maximum normalised power density  $\eta_{\max}$  against the normalised support-structure drag  $(A_s/A)C_D^*$  for various effective farm density  $\Lambda/C_{f0}$  ( $\zeta=0$  for all these results).



The maximum power coefficient  $C_p \max$  against the effective farm density  $\Lambda/C_{f0}$  for various normalised support-structure drag  $(A_s/A)C_D^*$  and  $\zeta$ .

- Wall-Modelled Large Eddy Simulations (DES with Spalart-Allmaras model)
- Constant streamwise pressure gradient for all cases
- Constant ground roughness length ( $z_0 = 0.05\text{m}$ )
- Periodic conditions applied to stream and spanwise directions
- Momentum sink method applied to the rotor ( $K = 0.5$ , no rotation) and support structure ( $K_s$ )

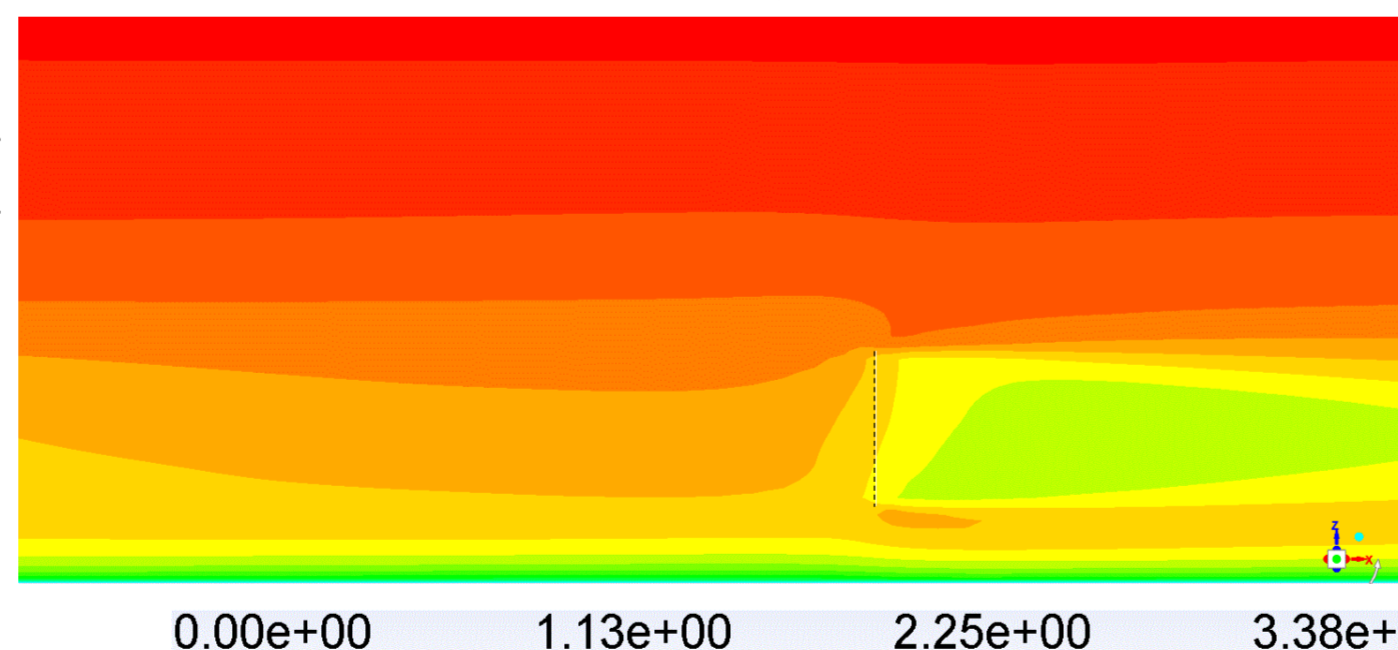


Instantaneous streamwise velocity [m/s] contours ( $K_s = 4$ ) on a vertical (centre of a turbine) and horizontal plan (hub height)

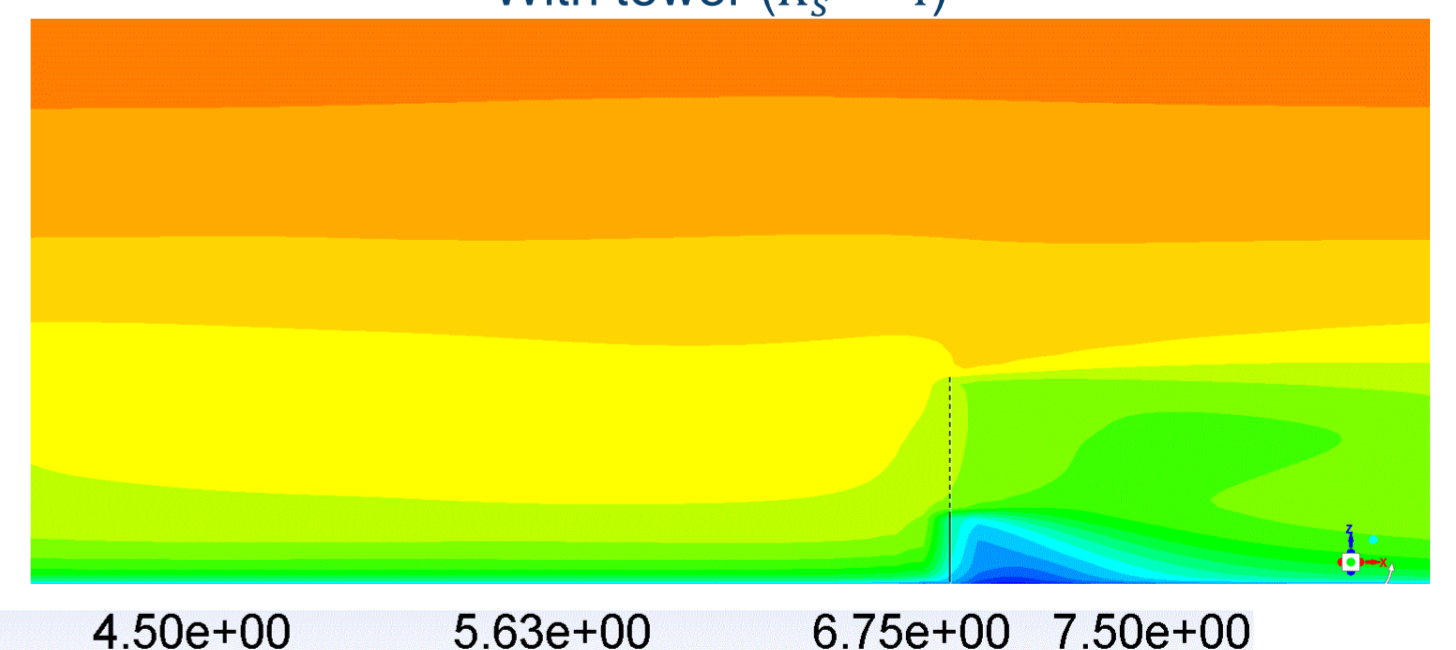
Summary of farm simulation results (Farm layer height  $H_F = 280\text{m}$ ,  $U_{F0} = 8.89\text{ m/s}$ ,  $K_s$  is the momentum loss factor assigned to the support structure)

Case	$K_s$	$C_{D(CFD)}^*$	$(A_s/A)C_D^*$
1	0	0	0
2	0.542	0.270	0.0321
3	1.129	0.448	0.0533
4	1.422	0.505	0.0600
5	1.716	0.537	0.0640
6	4	0.739	0.0879
7	5	0.774	0.0921

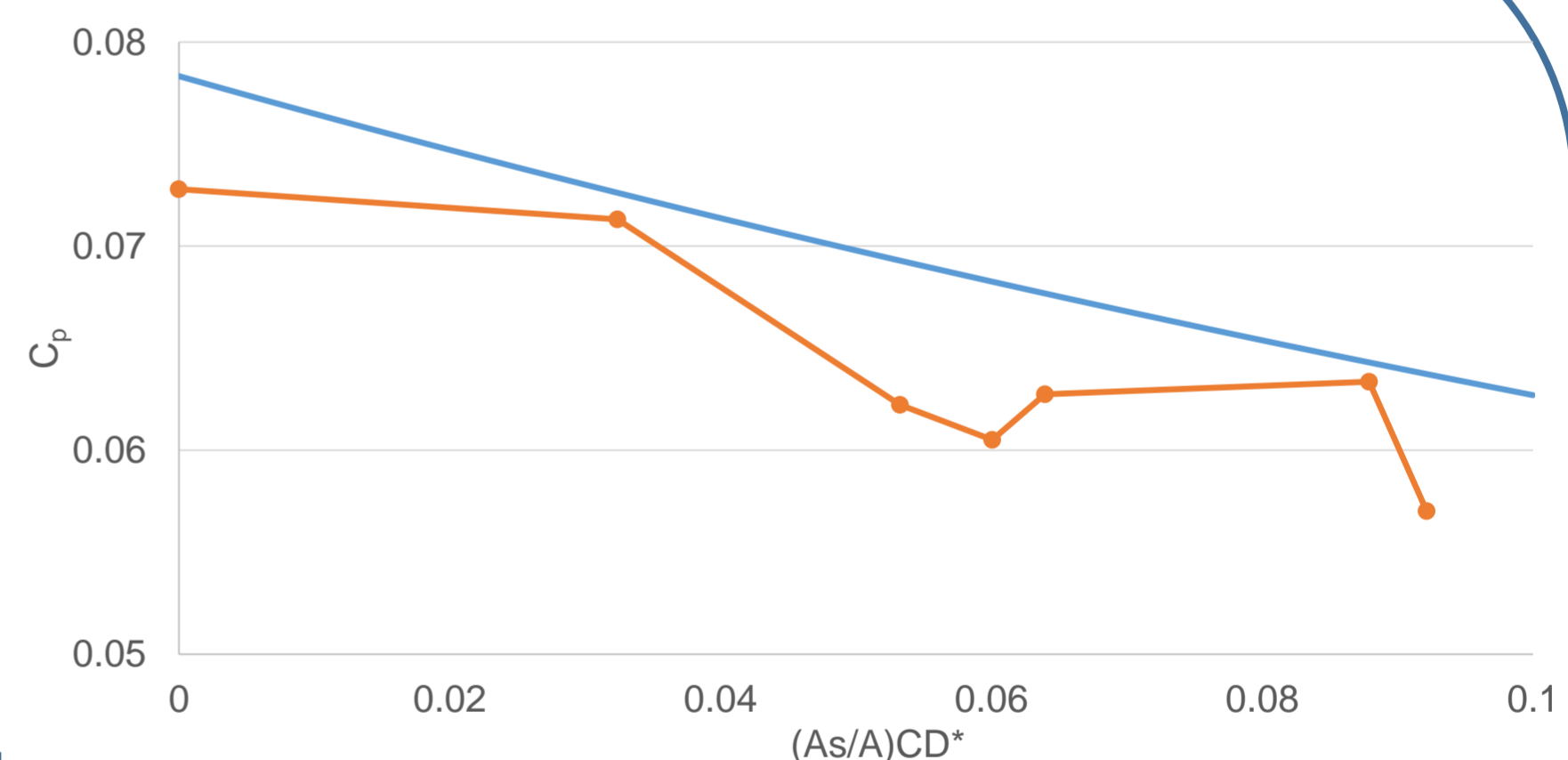
No tower



With tower ( $K_s = 4$ )



Time-averaged streamwise velocity [m/s] contours on a lateral plane across the centre of a turbine; dashed and solid lines show the rotor and tower positions, respectively.



Comparison of  $C_p$  between CFD (orange) and theoretical model (blue)

$\tau_{w(0)}$ : Wind-induced shear stress on the land/sea surface after (before) farm construction.  $S$ : Land/sea surface area per turbine.  $T$ : Turbine thrust.  $D$ : Support structure drag.  $\Delta p/\Delta p_0$ : Pressure gradient after/before wind farm construction.  $A$ : Rotor swept area.  $A_s$ : Frontal projected area of support structure.  $\alpha$ : Local flow reduction factor ( $U_T/U_F$ ).  $\beta$ : Farm flow reduction factor ( $U_F/U_{F0}$ ).  $U_T$ : Average wind speed across  $A$ .  $U_{F(0)}$ : Average wind speed across wind farm layer after (before) farm construction.  $\gamma$ : Empirical parameter (typically 2).  $\zeta$ : Environment-dependent empirical parameter.  $\Lambda$ : Farm density ( $A/S$ ).  $C_{f0}$ : Natural friction coefficient of the land/sea surface

Conclusions and Future study:

- The support structures have an increasingly important influence on the overall performance of a very large wind farm as the farm density (or the number of turbines installed in a given farm area) increases.
- Optimal rotor resistance decreases and therefore the relative importance of support-structure drag increases as the farm density increases.
- The environment-dependent parameter " $\zeta$ " has a greater effect on wind farm performance than the support-structure drag
- Fully-resolved turbine model simulations will be carried out for further theoretical model improvement and a collaboration work with Met Office is undergoing to extensively investigate the environment-dependent parameter " $\zeta$ ".